## EXAMPLES

1. The jet aircraft has a total mass of 22 Mg and a center of mass at $G$. Initially at take-off the engines provide a thrust of $2 T=4 \mathrm{kN}$ and $T^{\prime}=1.5 \mathrm{kN}$. Determine the acceleration of the plane and the normal reactions on the nose wheel and each of the two wing wheels located at $B$. Neglect the mass of the wheels and, due to low velocity, neglect any lift caused by the wings.


Data:
$m=22 \times 10^{6} \mathrm{gr}=22 \times 10^{3} \mathrm{~kg} \quad a_{G}=$ ?
$2 T=4000 N$
$N_{A}=$ ?
$T^{\prime}=1500 N \quad N_{B}=$ ?
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2. The pipe has a length of 3 m and a mass of 500 kg . It is attached to the back of the truck using a 0.6 m long chain $A B$. If the coefficient of kinetic fiction at $C$ is $\mu=0.4$, determine the acceleration of the truck if the angle $\theta=10^{\circ}$


SOLUTION

1) Geometry:

$$
\begin{aligned}
& \sin 10^{\circ}=\frac{a}{3} \Rightarrow a=0.52094 m \\
& \cos 10^{\circ}=\frac{b}{3} \Rightarrow b=2.9544 m
\end{aligned}
$$



1) $\sum F_{x}=m a_{G x} \Rightarrow T^{\prime}+2 T=m a_{G x}$ $1,500+4,000=22,000 a_{G x} \Rightarrow a_{G x}=0.25 \mathrm{~m} / \mathrm{s}^{2}$
2) $\quad \sum F_{y}=m a_{G y}=0 \Rightarrow N_{A}+2 N_{B}-22,000 \times 9.81=0$

$$
N_{A}+2 N_{B}=215,820
$$

3) $\sum M_{G}=0 \Rightarrow$
$N_{A}-N_{B}=1,058.33 \underset{25}{-T^{\prime}(2.5-1.2)-2 T(2.3-1.2)}-2 N_{B} \times 3+N_{A} \times 6=0$
$N_{\text {A }}=72,646 \mathrm{~N}=72.6 \mathrm{kN}$
$N_{B}=71,587 \mathrm{~N}=71.6 \mathrm{kN}$

3. The pipe has a mass of 460 kg and is held in place on the truck bed using the two boards $A$ and $B$. Determine the greatest acceleration of the truck so that the pipe begins to lose contact at $A$ and the bed of the truck and starts to pivot about $B$. Assume board $B$ will not slip on the bed of the truck, and the pipe is smooth. Also, what force does board $B$ exert on the pipe during the acceleration?


SOLUTION
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At the moment of interest
$\alpha=0$ and $\mathbf{N}=0$.

1) Equilibrium in the $x$ - direction
$\sum F_{x}=m a_{x} \Rightarrow P_{x}=m a_{x}$
2) Equilibrium in the y - direction
$\sum F_{y}=m a_{y} \Rightarrow P_{y}-W=0 \Rightarrow P_{y}=4513 \mathrm{~N}$
3) Equilibrium of moments about B
$\sum M_{G}=0 \Rightarrow P_{x} \times 0.4-P_{y} \times 0.3=0 \Rightarrow P_{x}=3384 \mathrm{~N}$
$a_{x}=7.36 \mathrm{~m} / \mathrm{s}^{2}$
1. The arm $B D E$ of the industrial robot manufactured by Cincinnati Milacron is activated by applying the torque of $M=50 \mathrm{~N} \cdot \mathrm{~m}$ to link $C D$. Determine the reactions at the pins $B$ and $D$ when the links are in the position shown and have an angular velocity of $2 \mathrm{rad} / \mathrm{s}$. The uniform arm $B D E$ has a mass of 10 kg and a center of mass at $G_{1}$. The container held in its grip at $E$ has a mass of 12 kg and a center of mass at $G_{2}$. Neglect the mass of links $A B$ and $C D$

|  |  |
| :--- | :--- | :--- |

3) Find $D_{y}$ using equilibrium in the y-direction

$$
B_{y}+D_{y}-W_{1}-W_{2}=-m_{1} a_{G_{1}}-m_{2} a_{G_{2}}
$$


$-567.54+D_{y}-98.1-117.72=-24-28.8$

$$
D_{y}=731 N
$$

4) Find $B_{x}$ using equilibrium in the x-direction. Because at this instant $a_{x}=a_{t}=0$ we have
$B_{x}+D_{x}=0 \Rightarrow B_{x}=-83.3 \mathrm{~N}$

Curvilinear Translation:
In a body subjected to a Curvilinear Translation all the points in the body travel along parallel curvilinear paths.
Here it is convenient to write the equations of motion in normal and tangential coordinates.

$$
\begin{aligned}
& \sum F_{n}=m a_{G n} \\
& \sum F_{t}=m a_{G t} \\
& \sum M_{G}=0
\end{aligned}
$$



If the summation of moments about $G$ is replaced by the summation about another point $B$ then we must account for the kinetic moments

$$
M_{B}=\sum\left(\mathscr{M}_{k}\right)_{B}=e \cdot\left(m a_{G t}\right)-h \cdot\left(m a_{G n}\right)
$$

EXAMPLES

This is a curvilinear translation

1) Element CD: Rotation about fixed point $C$

$$
\begin{gathered}
a_{D}=\omega^{2} r_{D / C}=2^{2} \times 0.6 \\
a_{D}=2.4 \mathrm{~m} / \mathrm{s}^{2}=a_{G} \\
\sum M_{C}=0 \Rightarrow D_{x} \times 0.6-50=0 \\
D_{x}=83.3 \mathrm{~N}
\end{gathered}
$$


2) In member BDE take $\sum M_{D}=\sum\left(\mathcal{M}_{k}\right)_{D}$, this eliminates $D_{y}$

$-B_{y} \times 0.22-98.1 \times 0.365-117.72 \times 1.1=(-10 \times 2.4) \times 0.365-(12 \times 2.4) \times 1.1$

$$
B_{y}=-568 N
$$

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2. The two $3-l b$ rods $E F$ and $H I$ are fixed (welded) to the link $A C$ at $E$. Determine the normal force $N_{E}$, the shear force $V_{E}$, and moment $M_{E}$, which the bar $A C$ exerts on $F E$ at $E$ if at the instant $\theta=30^{\circ} \operatorname{link} A B$ has an angular velocity $\omega=5 \mathrm{rad} / \mathrm{s}$ and an angular acceleration $\alpha=8 \mathrm{rad} / \mathrm{s}^{2}$ as shown

Data:
$W_{H I}=W_{E F}=3 l b$
$m_{H I}=m_{E F}=0.093168$ slug
$\omega=5 \mathrm{rad} / \mathrm{s}$
$\alpha=8 \mathrm{rad} / \mathrm{s}^{2}$
$N_{E}=$ ?
$V_{E}=$ ?
$M_{E}=$ ?


The bars EFHI are undergoing a curvilinear translation, therefore their angular velocity and acceleration must be zero.

1) Find the position of $G$ :
$G_{y}=0$
$G_{x}=\frac{3 l b \times(-1 f t)+3 l b \times(-2 f t)}{6 l b}=-1.5 f t$
2) Equilibrium in the $x$-direction:
$\sum F_{x}=N_{E}=2 m a_{G x}$
3) Equilibrium in the $y$-direction:

$$
\sum F_{y}=-2 W-V_{E}=2 m a_{G y}
$$


4) Equilibrium of moments about G :

$$
\sum M_{G}=M_{E}-V_{E} \times 1.5=0
$$

5) We must have $\mathbf{a}_{G}=\mathbf{a}_{A}$ and we can find $\mathbf{a}_{A}$ :

$\mathbf{a}_{A}=\boldsymbol{\alpha} \times \mathbf{r}_{A / B}-\omega^{2} \mathbf{r}_{A / B} \quad \mathbf{r}_{A / B}=-3 \cos 30^{\circ} \mathbf{i}+3 \sin 30^{\circ}$
$\mathbf{a}_{A}=(8 \mathbf{k}) \times(-2.5981 \mathbf{i}+1.5 \mathbf{j})-5^{2} \times(-2.5981 \mathbf{i}+1.5 \mathbf{j})$
$\mathbf{a}_{A}=53 \mathbf{i}-58.3 \mathbf{j}$

$$
N_{E}=9.87 \mathrm{lb}
$$

$$
V_{E}=-4.86 l b
$$

$$
M_{E}=-7.29 \mathrm{lb} \cdot f t
$$

The moment equation can be replaced by a summation about any point P lying inside or outside the body. In that case we must take into account the moments $\sum\left(\mathcal{M}_{k}\right)_{P}$ due to $I_{g} \alpha$, $m a_{G n}$ and $m a_{G t}$.
In many problems it is convenient to choose moments about $O$. This eliminates the unknown rection $\mathbf{F}_{o}$, and the kinetic moments become

$$
\sum M_{O}=\sum\left(\mathcal{M}_{k}\right)_{O}=m r_{G} a_{G t}+I_{G} \alpha
$$

Note that the component $m a_{G n}$ does not appear, because its line of action goes through the point $O$.
Furthermore, using $a_{G n}=r_{G} \alpha$ we have $\sum M_{O}=r_{G}^{2} m \alpha+I_{G} \alpha$ or $\sum M_{O}=\left(r_{G}^{2} m+I_{G}\right) \alpha$ and from the parallel axis theorem $I_{O}=I_{G}+m r_{G}^{2}$. Therefore we also have $\sum M_{O}=I_{O} \alpha$
2) Equilibrium of moments:

$$
\sum M_{O}=-5 \theta=0.10356 \alpha \Rightarrow \alpha=-48.281 \theta
$$

3) Kinematics: $\quad \alpha d \theta=\omega d \omega$

$$
\begin{gathered}
-\int_{\pi / 2}^{\pi / 4} 48.281 \theta d \theta=\int_{0}^{\omega} \omega d \omega \Rightarrow \frac{1}{2} \omega^{2}=-\left.24.141 \theta^{2}\right|_{\pi / 2} ^{\pi / 4} \\
\omega=9.45 \mathrm{rad} / \mathrm{s}
\end{gathered}
$$

2. The lightweight turbine consists of a rotor which is powered from a torque applied at its center. at the instant the rotor is horizontal it has an angular velocity of $15 \mathrm{rad} / \mathrm{s}$ and a clockwise angular acceleration of $8 \mathrm{rad} / \mathrm{s}^{2}$.
Determine the internal normal force, shear force and moment at a section through A. Assume the rotor is a 50 m long slender rod, having a mass of $3 \mathrm{~kg} / \mathrm{m}$.


$$
\begin{aligned}
& \text { b) Weight } B \text { : } \\
& \begin{array}{c}
\sum F_{y}=m_{B} a_{B y} \Rightarrow 5-T=0.15528 \times(\underset{\sim}{1.5 \times \alpha)} \\
T=5-0.23292 \times \alpha
\end{array}
\end{aligned}
$$

$$
\begin{gathered}
\alpha=0.826 \mathrm{rad} / \mathrm{s}^{2} \\
\text { Same as before }
\end{gathered}
$$


2) Consider each particle separate.

$$
\begin{aligned}
& \text { a) Spool } \sum_{M} M_{A}=I_{A} \alpha \\
& T \times 1.5=8.7345 \alpha \Rightarrow T=5.823 \alpha
\end{aligned}
$$



