

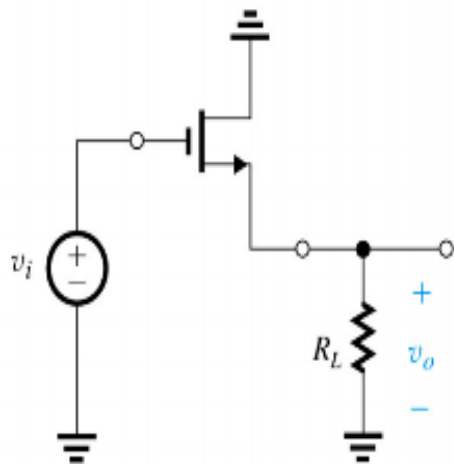
**ECE 523/421 - Analog Electronics**  
**University of New Mexico**  
**Solutions Homework 3**

**Problem 7.90**

Show that when  $r_o$  is taken into account, the voltage gain of the source follower becomes

$$G_v = \frac{v_o}{v_{sig}} = \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

Now, with  $R_L$  removed, the voltage gain is carefully measured and found to be 0.98. Then, when  $R_L$  is connected and its value is varied, it is found that the gain is halved at  $R_L = 500\Omega$ . If the amplifier remained linear throughout this measurement, what must the values of  $g_m$  and  $r_o$  be?



Because drain terminal is connected to ground  $R_L || r_o$   
 And using T-model.

We use a voltage division to determine  $v_o$

$$v_o = v_{sig} \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

From this voltage division we obtain  $G_v$

$$G_v = \frac{v_o}{v_{sig}} = \frac{R_L || r_o}{(R_L || r_o) + \frac{1}{g_m}}$$

When we remove  $R_L$

$$G_v = \frac{r_o}{(r_o) + \frac{1}{g_m}}$$

$$G_v = 0.98$$

With  $R_L = 500\Omega$

$$G_v = \frac{500 || r_o}{(500 || r_o) + \frac{1}{g_m}}$$

$$G_v = 0.49$$

From the equation without  $R_L$  we found

$$\frac{r_o}{49} = \frac{1}{g_m}$$

Substituting  $\frac{r_o}{49} = \frac{1}{g_m}$  in equation with  $R_L = 500\Omega$

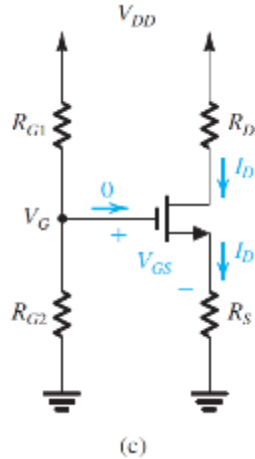
$$r_o = 25k\Omega$$

Therefore

$$g_m = \frac{49}{r_o}$$
$$g_m = 1.96 \text{ mA/V}$$

### Problem 7.94

In an electronic instrument using the biasing scheme shown in Fig. 7.48(c), a manufacturing error reduces  $R_S$  to zero. Let  $V_{DD} = 15\text{ V}$ ,  $R_{G1} = 10\text{ M}\Omega$ , and  $R_{G2} = 5.1\text{ M}\Omega$ . What is the value of  $V_G$  created? If supplier specifications allow  $k_n$  to vary from 0.2 to 0.3  $\text{mA/V}^2$  and  $V_t$  to vary from 1.0 V to 1.5 V, what are the extreme values of  $I_D$  that may result? What value of  $R_S$  should have been installed to limit the maximum value of  $I_D$  to 1.5 mA? Choose an appropriate standard 5% resistor value (refer to Appendix J). What extreme values of current now result?



Using voltage division to calculate  $V_G$

$$V_G = V_{DD} \frac{R_{G2}}{R_{G2} + R_{G1}}$$

$$V_G = 15 \frac{5.1}{5.1 + 10} = 5.07\text{ V}$$

For calculating  $I_D$  we use the equation for drain current

$$I_D = \frac{1}{2} (k_n') \left( \frac{W}{L} \right) (5.07 - V_t)^2$$

For  $I_{D\text{MIN}}$  we use  $k_n = 0.2$  and  $V_t = 1.5\text{ V}$

$$I_{D\text{MIN}} = \frac{1}{2} (0.2) (5.07 - 1.5)^2$$

$$I_{D\text{MIN}} = 1.27\text{ mA}$$

For  $I_{D\text{MAX}}$  we use  $k_n = 0.3$  and  $V_t = 1\text{ V}$

$$I_{D\text{MAX}} = \frac{1}{2} (0.3) (5.07 - 1)^2$$

$$I_{D\text{MAX}} = 2.48\text{ mA}$$

Using the equation for drain current for calculating the new  $V_{GS}$  using the MAX values for  $k_n = 0.3$  and  $V_t = 1\text{ V}$  because this will be the new MAX drain current.

$$I_D = \frac{1}{2} (k_n') \left( \frac{W}{L} \right) (V_{OV})^2$$

$$V_{OV} = 3.16\text{ V}$$

$$V_{GS} = 4.16\text{ V}$$

Then we calculate  $V_S$

$$\begin{aligned}V_S &= V_G - V_{GS} \\V_S &= 5.07 - 4.16 \\V_S &= 0.91V\end{aligned}$$

Knowing  $V_S$  we can simply calculate  $R_S$

$$\begin{aligned}R_S &= \frac{V_S}{I_{DS}} = \frac{0.91}{1.5mA} \\R_S &= 606.6\Omega \\R_S &\cong 620\Omega\end{aligned}$$

### Problem 7.103

Figure P7.103 shows a variation of the feedback-bias circuit of Fig. 7.50. Using a 5V supply with an NMOS transistor for which  $V_t = 0.8\text{ V}$ ,  $k_n = 8\text{ mA/V}^2$ , and  $\lambda=0$ , provide a design that biases the transistor at  $I_D = 1\text{ mA}$ , with  $V_{DS}$  large enough to allow saturation operation for a 2V negative signal swing at the drain. Use  $22\text{M}\Omega$  as the largest resistor in the feedback-bias network. What values of  $R_D$ ,  $R_{G1}$ , and  $R_{G2}$  have you chosen? Specify all resistors to two significant digits.

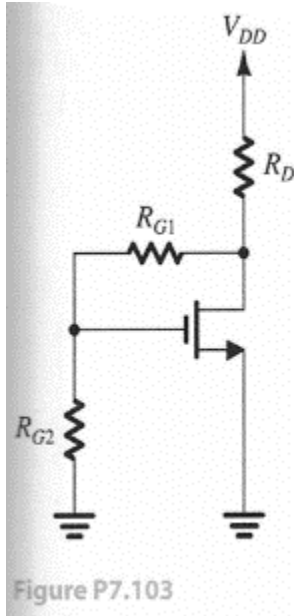


Figure P7.103

Using the equation for the drain current for calculating  $V_{GS}$  and then  $V_G$

$$I_D = \frac{1}{2} (k_n') \left( \frac{W}{L} \right) (V_{GS} - V_t)^2$$

$$1\text{m} = \frac{1}{2} (8\text{m}) (V_{GS} - 0.8)^2$$

$$V_{GS} = 1.3\text{V}$$

$$V_G = 1.3\text{V}$$

Using the condition for  $V_{DSMIN}$

$$V_{DSMIN} = V_{GS} - V_t = 0.5\text{V}$$

$$V_{DS} = V_{DSMIN} + 2 = 2.5\text{V}$$

Assuming  $R_{G2} = 22\text{M}\Omega$

$$I = \frac{V_G}{R_{G2}} = \frac{1.3}{22\text{M}\Omega} = 5.91 \times 10^{-8}\text{ A}$$

Calculating  $R_{G1}$

$$R_{G1} = \frac{V_{DS} - V_G}{I} = \frac{2.5 - 1.3}{5.91 \times 10^{-8}} = 20.3\text{M}\Omega$$

$$R_{G1} = 20\text{M}\Omega$$

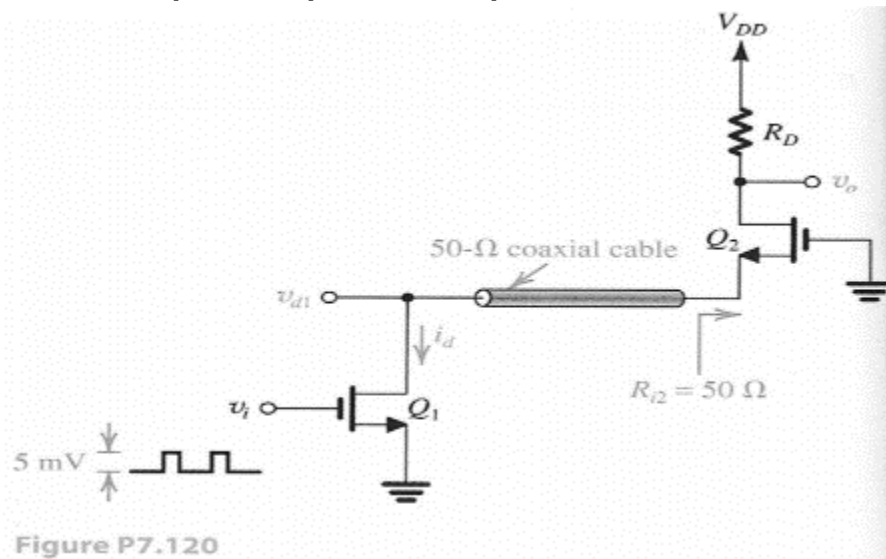
Calculating  $R_D$

$$R_D = \frac{V_{DD} - V_{DS}}{I_D} = \frac{5 - 2.5}{1 \times 10^{-3}} = 2.5\text{k}\Omega$$

$$R_D = 2.5\text{k}\Omega$$

### Problem 7.120

Figure P7.120 shows a scheme for coupling and amplifying a high-frequency pulse signal. The circuit utilizes two MOSFETs whose bias details are not shown and a 50Ω coaxial cable. Transistor Q1 operates as a CS amplifier and Q2 as a CG amplifier. For proper operation, transistor Q2 is required to present a 50Ω resistance to the cable. This situation is known as “proper termination” of the cable and ensures that there will be no signal reflection coming back on the cable. When the cable is properly terminated, its input resistance is 50Ω. What must  $g_{m2}$  be? If Q1 is biased at the same point as Q2, what is the amplitude of the current pulses in the drain of Q1? What is the amplitude of the voltage pulses at the drain of Q1? What value of  $R_D$  is required to provide 1-V pulses at the drain of Q2?



Calculating  $g_{m2}$

$$R_{i2} = \frac{1}{g_{m2}} = 50\Omega$$

$$g_{m2} = \frac{1}{R_{i2}} = 20 \text{ mA/V}$$

If Q1 is biased at the same point as Q2 then  $g_{m2} = g_{m1}$

$$i_{D1} = g_{m1} v_i = 20 \times 5 = 1 \times 10^{-4} \text{ A}$$

$$i_{D1} = 0.1 \text{ mA}$$

$$v_{D1} = i_{D1} \times 50 = 5 \times 10^{-3} \text{ V}$$

$$v_{D1} = 5 \text{ mV}$$

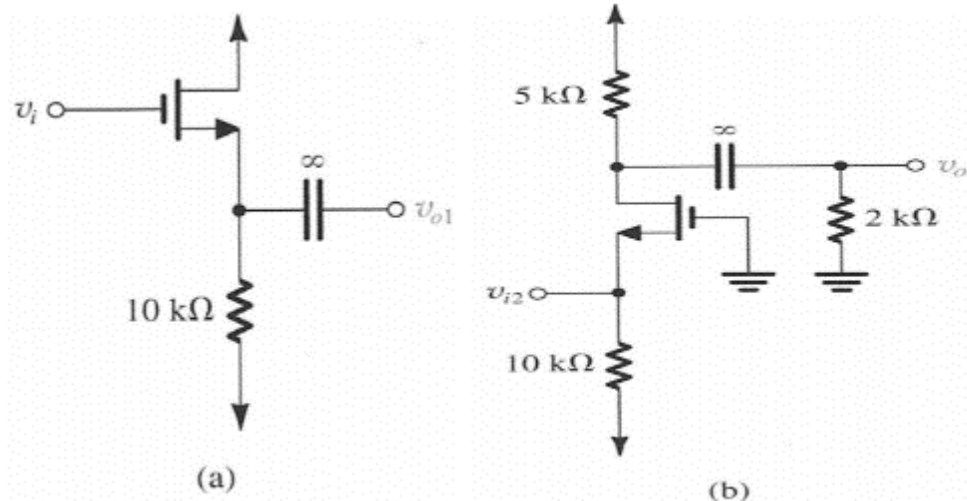
In order to have  $v_{D2} = v_o = 1V$

$$R_D = \frac{v_o}{i_D} = \frac{1}{0.1mA} = 10k\Omega$$

$$R_D = 10k\Omega$$

**Problem 7.122**

- (a) The NMOS transistor in the source-follower circuit of Fig. P7.122(a) has  $g_m = 10 \text{ mA/V}$  and a large  $r_o$ . Find the open-circuit voltage gain and the output resistance.
- (b) The NMOS transistor in the common-gate amplifier of Fig. P7.122(b) has  $g_m = 10 \text{ mA/V}$  and a large  $r_o$ . Find the input resistance and the voltage gain.
- (c) If the output of the source follower in (a) is connected to the input of the common-gate amplifier in (b), use the results of (a) and (b) to obtain the overall voltage gain  $v_o/v_i$ .



- (a) For the source follower using T model and voltage division

$$v_{o1} = v_i \frac{R_S}{R_S + \frac{1}{g_m}} = v_i \frac{10k}{10k + \frac{1}{10m}} = v_i \frac{10k}{10.1k}$$

$$G_v = 0.99$$

$$R_{out} = \frac{1}{g_m} || r_o$$

Since  $r_o$  is very large

$$R_{out} = \frac{1}{g_m} = \frac{1}{10m} = 100\Omega$$

- (b) For the common gate circuit and since  $r_o$  is very large

$$R_{in} = \frac{1}{g_m}$$



$$R_{in} = \frac{1}{g_m} = \frac{1}{10m} = 100\Omega$$

Using T model and voltage division

$$v_o = v_{i2} \frac{R_D || R}{\frac{1}{g_m}} = v_i \frac{5k || 2k}{\frac{1}{10m}}$$

$$G_v = 14.3$$

(c) If we connect both stages together. For the first step

$$A_{v1} = A_{v1} \frac{R_L}{R_L + R_{out}}$$

Where  $R_L$  is  $R_{in}$  of the second stage

$$A_{v1} = 1 \frac{100}{100 + 100}$$

$$A_{v1} = 0.5$$

For the second stage

$$A_{v2} = 14.3$$

Overall gain

$$A_v = A_{v1} A_{v2} = 7.15$$

**Problem 7.123**

The MOSFET in the amplifier circuit of Fig. P7.123 has  $V_t = 0.6\text{ V}$ ,  $k_n = 5\text{ mA/V}^2$ , and  $V_A = 60\text{ V}$ . The signal  $v_{\text{sig}}$  has a zero average.

- It is required to bias the transistor to operate at an overdrive voltage  $V_{OV} = 0.2\text{ V}$ . What must the dc voltage at the drain be? Calculate the dc drain current  $I_D$  taking into account  $V_A$ . Now, what value must the drain resistance  $R_D$  have?
- Calculate the values of  $g_m$  and  $r_o$  at the bias point established in (a).
- Using the small-signal equivalent circuit of the amplifier, show that the voltage gain is given by

$$\frac{v_o}{v_{\text{sig}}} = - \frac{R_2/R_1}{1 + \frac{R_2/R_1}{g_m(R_D \parallel r_o \parallel R_2)(1 - 1/g_m R_2)}}$$

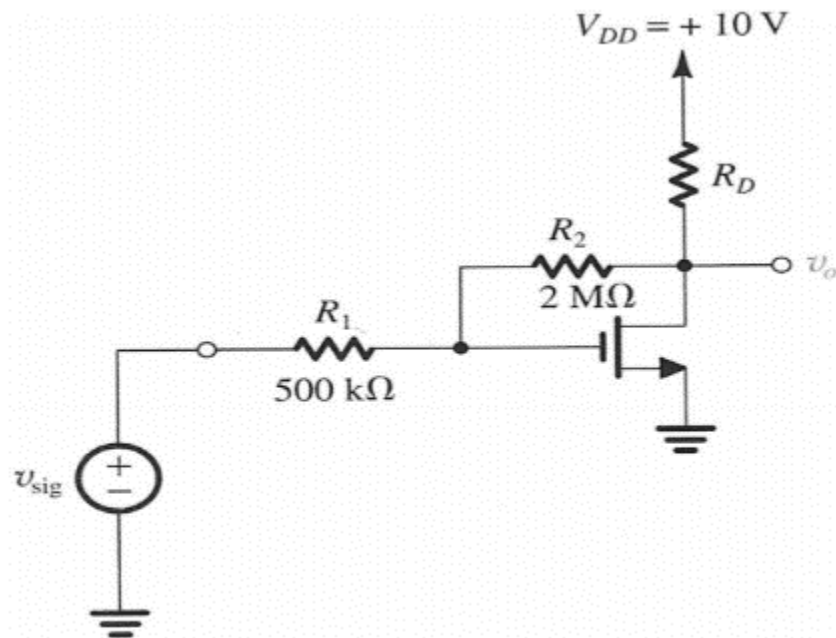


Figure P7.123

a) At DC,  $v_{sig} = 0$  shortcircuit. Also

$$V_{GS} = V_{OV} + V_t$$
$$V_{GS} = 0.8V$$

From the voltage division between  $R_1$  and  $R_2$

$$V_{GS} = V_D \frac{R_1}{R_1 + R_2}$$
$$V_D = 4V$$

Using the equation for the drain current taking in account VA

$$I_D = \frac{1}{2} (k_n) (V_{OV})^2 \left( 1 + \frac{V_{DS}}{VA} \right)$$
$$I_D = \frac{1}{2} (5) (0.2)^2 \left( 1 + \frac{4}{60} \right)$$
$$I_D = 0.107 \text{ mA}$$

Now we have the voltage and current going through  $R_D$

$$R_D = \frac{V_{DD} - V_D}{I_D} = \frac{10 - 4}{0.107 \text{ mA}}$$
$$R_D = 56 \text{ k}\Omega$$

b) The equation for  $g_m$

$$g_m = \frac{2I_D}{V_{ov}} = \frac{2 \times 0.107 \text{ mA}}{0.2}$$
$$g_m = 1.07 \text{ mA/V}$$

The equation for

$$r_o = \frac{VA}{I_D} = \frac{60}{0.107 \text{ mA}}$$
$$r_o = 560.7 \text{ k}\Omega$$