

- (e) Sketch a Bode plot for the gain of this amplifier. What does the plot tell you about the gain at dc? Does this make sense? Why or why not?

D 10.6 Figure P10.6 shows a CS amplifier biased by a constant-current source I . Let $R_{\text{sig}} = 0.5 \text{ M}\Omega$, $R_G = 2 \text{ M}\Omega$, $g_m = 3 \text{ mA/V}$, $R_D = 20 \text{ k}\Omega$, and $R_L = 10 \text{ k}\Omega$. Find A_M . Also,

design the coupling and bypass capacitors to locate the three low-frequency poles at 100 Hz, 10 Hz, and 1 Hz. Use a minimum total capacitance, with the capacitors specified only to a single significant digit. What value of f_L results?

D 10.7 Figure P10.7 shows a current-biased CE amplifier operating at $100 \mu\text{A}$ from $\pm 3\text{-V}$ power supplies. It employs

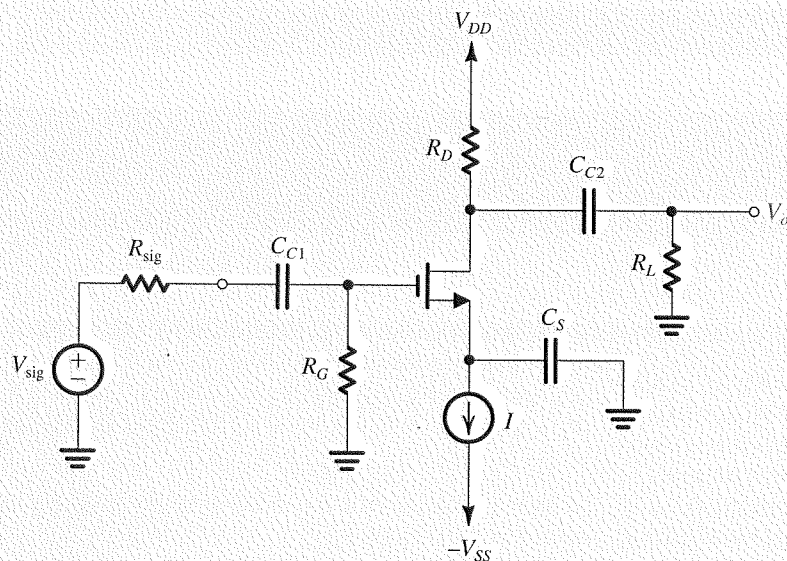


Figure P10.6

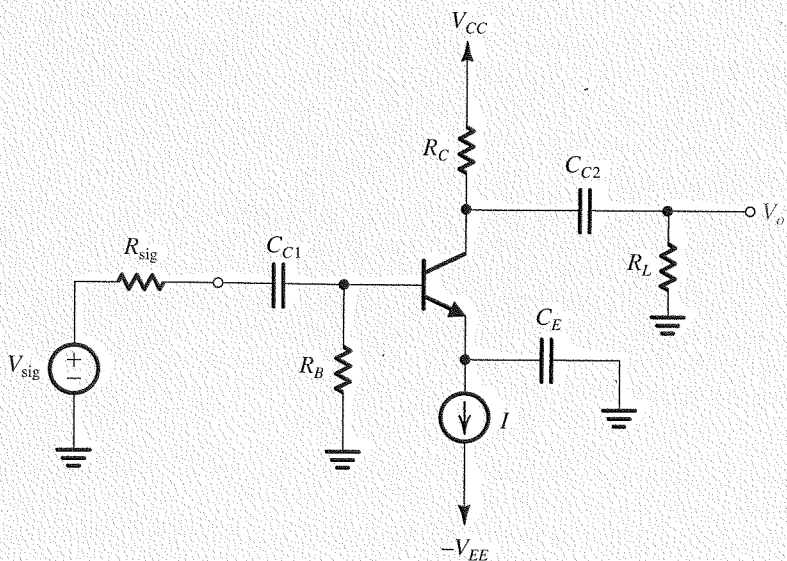


Figure P10.7

Section 10.4: Useful Tools for the Analysis of the High-Frequency Response of Amplifiers

10.51 A direct-coupled amplifier has a low-frequency gain of 40 dB, poles at 2 MHz and 20 MHz, a zero on the negative real axis at 200 MHz, and another zero at infinite frequency. Express the amplifier gain function in the form of Eqs. (10.70) and (10.71), and sketch a Bode plot for the gain magnitude. What do you estimate the 3-dB frequency f_H to be?

10.52 An amplifier with a dc gain of 60 dB has a single-pole, high-frequency response with a 3-dB frequency of 100 kHz.

- Give an expression for the gain function $A(s)$.
- Sketch Bode diagrams for the gain magnitude and phase.
- What is the gain–bandwidth product?
- What is the unity-gain frequency?
- If a change in the amplifier circuit causes its transfer function to acquire another pole at 1 MHz, sketch the resulting gain magnitude and specify the unity-gain frequency. Note that this is an example of an amplifier with a unity-gain bandwidth that is different from its gain–bandwidth product.

10.53 Consider an amplifier whose $F_H(s)$ is given by

$$F_H(s) = \frac{1}{\left(1 + \frac{s}{\omega_{p1}}\right)\left(1 + \frac{s}{\omega_{p2}}\right)}$$

with $\omega_{p1} < \omega_{p2}$. Find the ratio ω_{p2}/ω_{p1} for which the value of the 3-dB frequency ω_H calculated using the dominant-pole approximation differs from that calculated using the root-sum-of-squares formula (Eq. 10.77) by:

- 10%
- 1%

10.54 The high-frequency response of a direct-coupled amplifier having a dc gain of -1000 V/V incorporates zeros at ∞ and 10^4 rad/s (one at each frequency) and poles at 10^3 rad/s and 10^5 rad/s (one at each frequency). Write an expression for the amplifier transfer function. Find ω_H using

- the dominant-pole approximation
- the root-sum-of-squares approximation (Eq. 10.77).

If a way is found to lower the frequency of the finite zero to 10^3 rad/s, what does the transfer function become? What is the 3-dB frequency of the resulting amplifier?

10.55 A direct-coupled amplifier has a dominant pole at 1000 rad/s and three coincident poles at a much higher frequency. These nondominant poles cause the phase lag of the amplifier at high frequencies to exceed the 90° angle due to the dominant pole. It is required to limit the excess phase at $\omega = 10^7$ rad/s to 30° (i.e., to limit the total phase angle to -120°). Find the corresponding frequency of the nondominant poles.

10.56 An IC CS amplifier has $g_m = 2$ mA/V, $C_{gs} = 30$ fF, $C_{gd} = 5$ fF, $C_L = 30$ fF, $R'_{sig} = 10$ k Ω , and $R'_L = 20$ k Ω . Use the method of open-circuit time constants to obtain an estimate for f_H . Also, find the frequency of the transmission zero, f_Z .

10.57 For a particular amplifier modeled by the circuit of Fig. 10.18(a), $g_m = 5$ mA/V, $R_{sig} = 150$ k Ω , $R_G = 0.65$ M Ω , $R'_L = 10$ k Ω , $C_{gs} = 2$ pF, and $C_{gd} = 0.5$ pF. There is also a load capacitance of 30 pF. Find the corresponding midband voltage gain, the open-circuit time constants, and an estimate of the 3-dB frequency.

10.58 Consider the high-frequency response of an amplifier consisting of two identical stages in cascade, each with an input resistance of 10 k Ω and an output resistance of 2 k Ω . The two-stage amplifier is driven from a 10-k Ω source and drives a 1-k Ω load. Associated with each stage is a parasitic input capacitance (to ground) of 10 pF and a parasitic output capacitance (to ground) of 2 pF. Parasitic capacitances of 10 pF and 7 pF also are associated with the signal-source and load connections, respectively. For this arrangement, find the three poles and estimate the 3-dB frequency f_H .

10.59 A CS amplifier that can be represented by the equivalent circuit of Fig. 10.24 has $C_{gs} = 2$ pF, $C_{gd} = 0.1$ pF, $C_L = 2$ pF, $g_m = 4$ mA/V, and $R'_{sig} = R'_L = 20$ k Ω . Find the midband gain A_M , the input capacitance C_{in} using the Miller approximation, and hence an estimate of the 3-dB frequency f_H . Also, obtain another estimate of f_H using open-circuit time constants. Which of the two estimates is more appropriate and why?

D 10.60 For a CS amplifier with $g_m = 5$ mA/V, $C_{gs} = 5$ pF, $C_{gd} = 1$ pF, $C_L = 5$ pF, $R'_{sig} = 10$ k Ω , and $R'_L = 10$ k Ω , find τ_H and f_H . What is the percentage of τ_H that is caused by the interaction of R'_{sig} with the input capacitance? To what value must R'_{sig} be lowered in order to double f_H ?

D 10.61 For the CS amplifier in Example 10.8, find the value of the additional capacitance to be connected at the output node in order to lower f_H to 100 MHz.

10.91 A differential amplifier is biased by a current source having an output resistance of $1\text{ M}\Omega$ and an output capacitance of 1 pF . The differential gain exhibits a dominant pole at 2 MHz . What are the poles of the CMRR?

10.92 A current-mirror-loaded MOS differential amplifier is biased with a current source $I = 0.2\text{ mA}$. The two NMOS transistors of the differential pair are operating at $V_{OV} = 0.2\text{ V}$, and the PMOS devices of the mirror are operating at $|V_{OV}| = 0.2\text{ V}$. The Early voltage $V_{An} = |V_{Ap}| = 10\text{ V}$. The total capacitance at the input node of the mirror is 0.1 pF and that at the output node of the amplifier is 0.2 pF . Find the dc value and the frequencies of the poles and zero of the differential voltage gain.

10.93 Consider the current-mirror-loaded CMOS differential amplifier of Fig. 10.37(a) for the case of all transistors operated at the same $|V_{OV}|$ and having the same $|V_A|$. Also let the total capacitance at the output node (C_L) be four times the total capacitance at the input node of the current mirror C_m . Give expressions for A_d , f_{p1} , f_{p2} , and f_z . Hence show that $f_{p2}/f_{p1} = 4A_d$ and $f_z = g_m/2\pi C_L$. For $V_A = 20\text{ V}$, $V_{OV} = 0.2\text{ V}$, $I = 0.2\text{ mA}$, $C_L = 100\text{ fF}$, and $C_m = 25\text{ fF}$, find the dc value of A_d , and the value of f_{p1} , f_z , f_{p2} , and f_z and sketch a Bode plot for $|A_d|$.

***10.94** For the current mirror in Fig. P10.94, derive an expression for the current transfer function $I_o(s)/I_i(s)$ taking into account the BJT internal capacitances and neglecting r_x and r_o . Assume the BJTs to be identical. Observe that a signal ground appears at the collector of Q_2 . If the mirror is biased at 1 mA and the BJTs at this operating point are characterized by $f_T = 500\text{ MHz}$, $C_\mu = 2\text{ pF}$, and $\beta_0 = 100$, find the frequencies of the pole and zero of the transfer function.

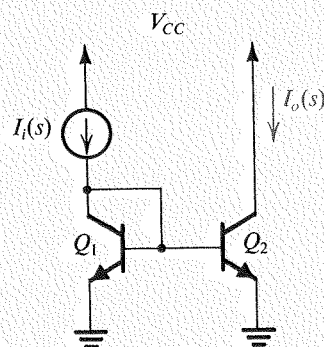


Figure P10.94

Section 10.8: Other Wideband Amplifier Configurations

10.95 Consider the case of a discrete-circuit CS amplifier in which a source-degeneration resistance is utilized to control the bandwidth. Assume that r_o is very large and C_L is negligibly small. Adapt the formulas given in the text for this case and thus give the expressions for A_M and f_H . Let $R_{sig} = 100\text{ k}\Omega$, $g_m = 5\text{ mA/V}$, $R_L = 5\text{ k}\Omega$, $C_{gs} = 10\text{ pF}$, and $C_{gd} = 2\text{ pF}$. Find $|A_M|$, f_H , and the gain-bandwidth product for these three cases: $R_s = 0, 100\text{ }\Omega$, and $200\text{ }\Omega$.

10.96 A CS amplifier is specified to have $g_m = 5\text{ mA/V}$, $r_o = 40\text{ k}\Omega$, $C_{gs} = 2\text{ pF}$, $g_{gd} = 0.1\text{ pF}$, $C_L = 1\text{ pF}$, $R_{sig} = 20\text{ k}\Omega$, and $R_L = 40\text{ k}\Omega$.

- Find the low-frequency gain A_M , and use open-circuit time constants to estimate the 3-dB frequency f_H . Hence determine the gain-bandwidth product.
- If a $400\text{-}\Omega$ resistance is connected in the source lead, find the new values of $|A_M|$, f_H , and the gain-bandwidth product.

D 10.97 (a) Use the approximate expression in Eq. (10.156) to determine the gain-bandwidth product of a CS amplifier with a source-degeneration resistance. Assume $C_{gd} = 0.2\text{ pF}$ and $R_{sig} = 100\text{ k}\Omega$.

- If a low-frequency gain of 20 V/V is required, what f_H corresponds?
- For $g_m = 5\text{ mA/V}$, $A_0 = 100\text{ V/V}$, and $R_L = 20\text{ k}\Omega$, find the required value of R_s .

10.98 For the CS amplifier with a source-degeneration resistance R_s , show for $R_{sig} \gg R_s$, $r_o \gg R_s$, and $R_L = r_o$ that

$$A_M = \frac{-A_0}{2+k}$$

and

$$\tau_H \simeq \frac{C_{gs}R_{sig}}{1+(k/2)} + C_{gd}R_{sig} \left(1 + \frac{A_0}{2+k} \right) + (C_L + C_{gd})r_o \left(\frac{1+k}{2+k} \right)$$

where $k \equiv g_m R_s$.

D *10.99 It is required to generate a table of $|A_M|$, f_H , and f_z versus $k \equiv g_m R_s$ for a CS amplifier with a source-degeneration resistance R_s . The table should have entries for $k = 0, 1, 2, \dots, 15$. The amplifier is specified to have $g_m = 5\text{ mA/V}$, $r_o = 40\text{ k}\Omega$, $R_L = 40\text{ k}\Omega$, $R_{sig} = 20\text{ k}\Omega$, $C_{gs} = 2\text{ pF}$, $C_{gd} = 0.1\text{ pF}$, and $C_L = 1\text{ pF}$. Use the formulas

***10.106** Figure P10.106 shows an amplifier formed by cascading two CS stages. Note that the input bias voltage is not shown. Each of Q_1 and Q_2 is operated at an overdrive voltage of 0.2 V, and $|V_A| = 10$ V. The transistor capacitances are as follows: $C_{gs} = 20$ fF, $C_{gd} = 5$ fF, and $C_{db} = 5$ fF. The signal-source resistance $R_{sig} = 10$ k Ω .

- Find the dc voltage gain.
- Use the method of open-circuit time constants to determine an estimate for the 3-dB frequency f_H .

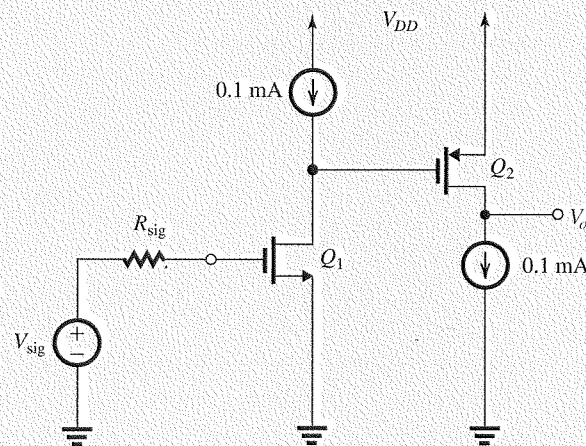


Figure P10.106

****10.107** Consider the BiCMOS amplifier shown in Fig. P10.107. The BJT has $|V_{BE}| = 0.7$ V, $\beta = 200$, $C_\mu = 0.8$ pF, and $f_T = 600$ MHz. The NMOS transistor has $V_t = 1$ V, $k'_n W/L = 2$ mA/V², and $C_{gs} = C_{gd} = 1$ pF.

- Consider the dc bias circuit. Neglect the base current of Q_2 in determining the current in Q_1 . Find the dc bias currents in Q_1 and Q_2 , and show that they are approximately 100 μ A and 1 mA, respectively.
- Evaluate the small-signal parameters of Q_1 and Q_2 at their bias points.
- Consider the circuit at midband frequencies. First, determine the small-signal voltage gain V_o/V_i . (Note that R_G can be neglected in this process.) Then use Miller's theorem on R_G to determine the amplifier input resistance R_{in} . Finally, determine the overall voltage gain V_o/V_{sig} . Assume r_o of both transistors to be very large.
- Consider the circuit at low frequencies. Determine the frequency of the poles due to C_1 and C_2 , and hence estimate the lower 3-dB frequency, f_L .
- Consider the circuit at higher frequencies. Use Miller's theorem to replace R_G with a resistance at the input. (The one at the output will be too large to matter.) Use open-circuit time constants to estimate f_H .

*****10.108** In each of the six circuits in Fig. P10.108, let $\beta = 100$, $C_\mu = 2$ pF, and $f_T = 400$ MHz, and neglect r_x and r_o . Calculate the midband gain A_M and the 3-dB frequency f_H .

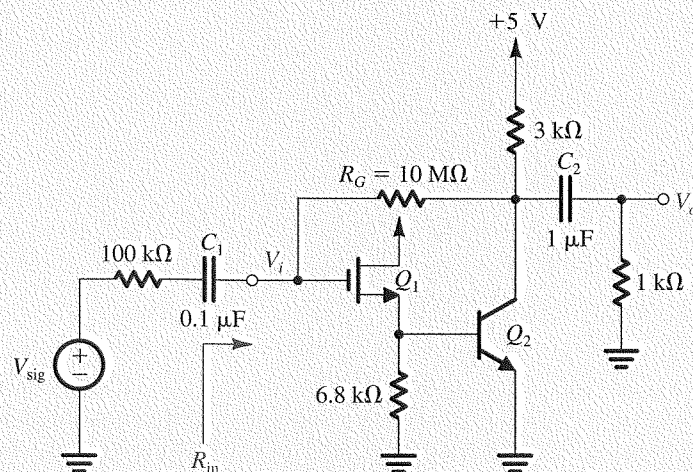


Figure P10.107